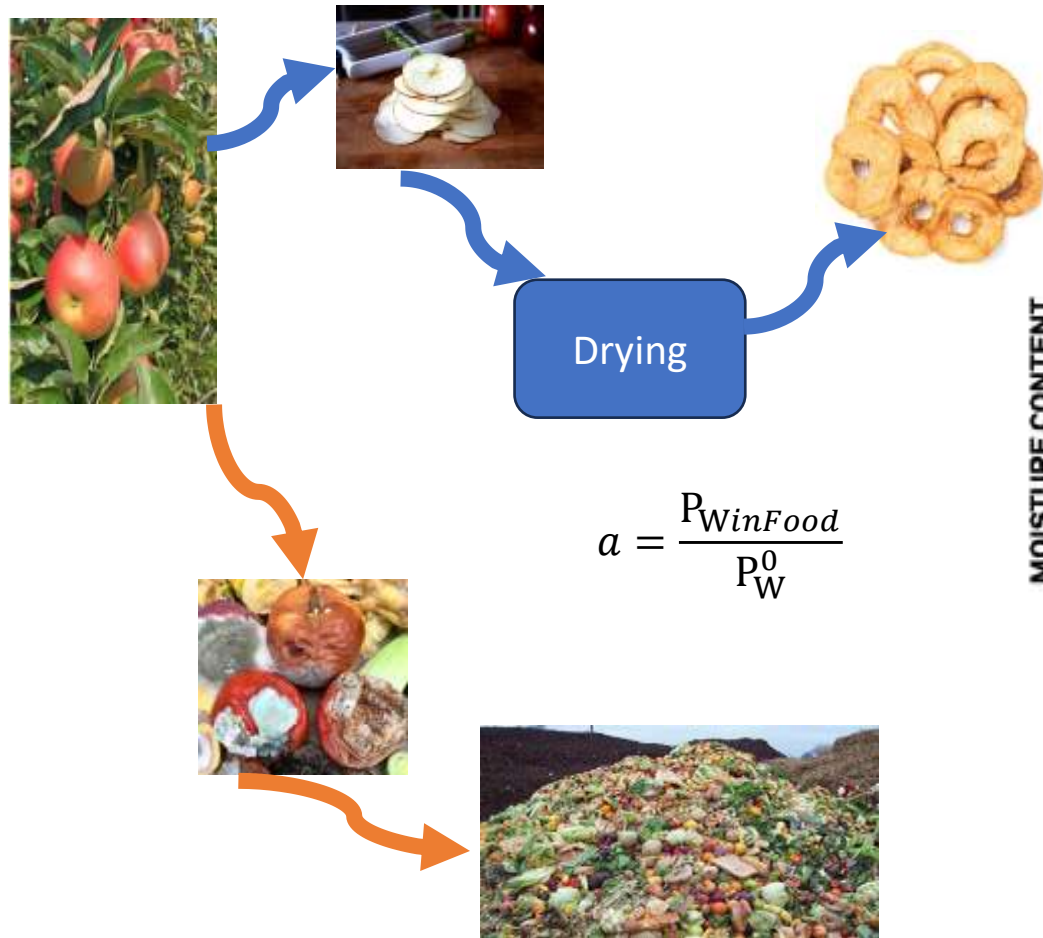




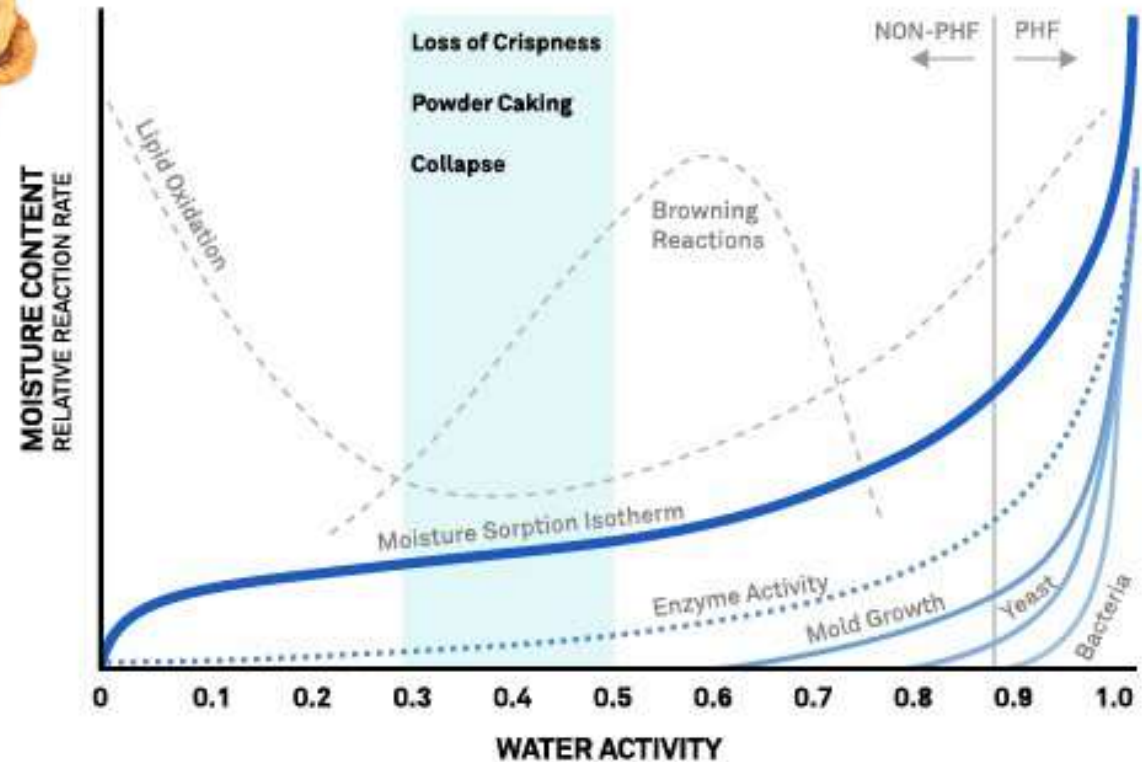
Food drying: Effect of process conditions and use of renewable energy sources

Juma Haydary, Department of Chemical and Biochemical
Engineering, Slovak University of Technology in Bratislava

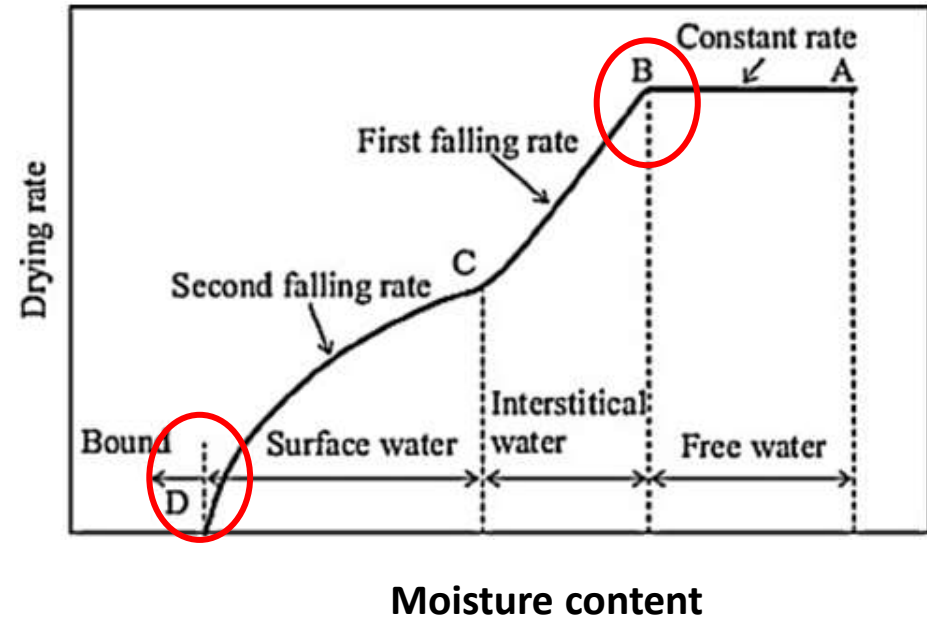
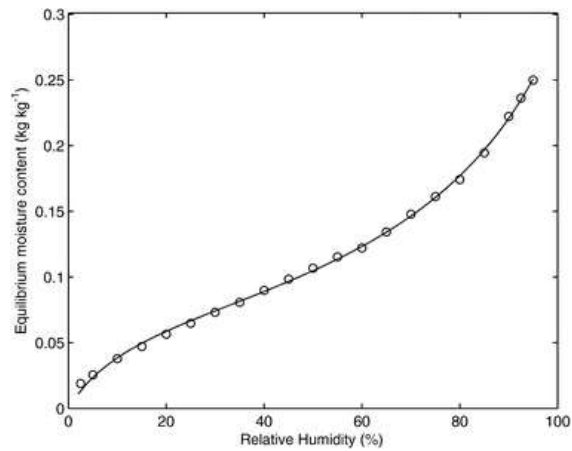
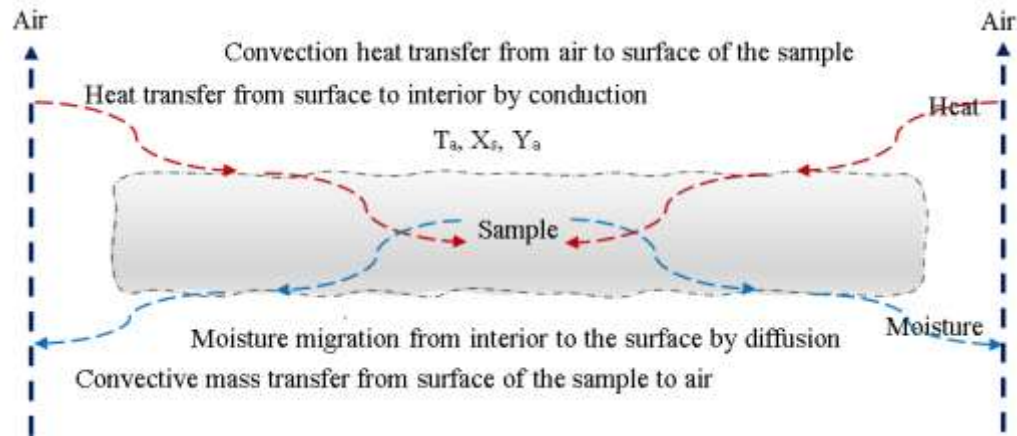
Drying as a method of food preservation



WATER ACTIVITY - STABILITY DIAGRAM



Drying mechanism, drying equilibrium



Energy requirement of drying process

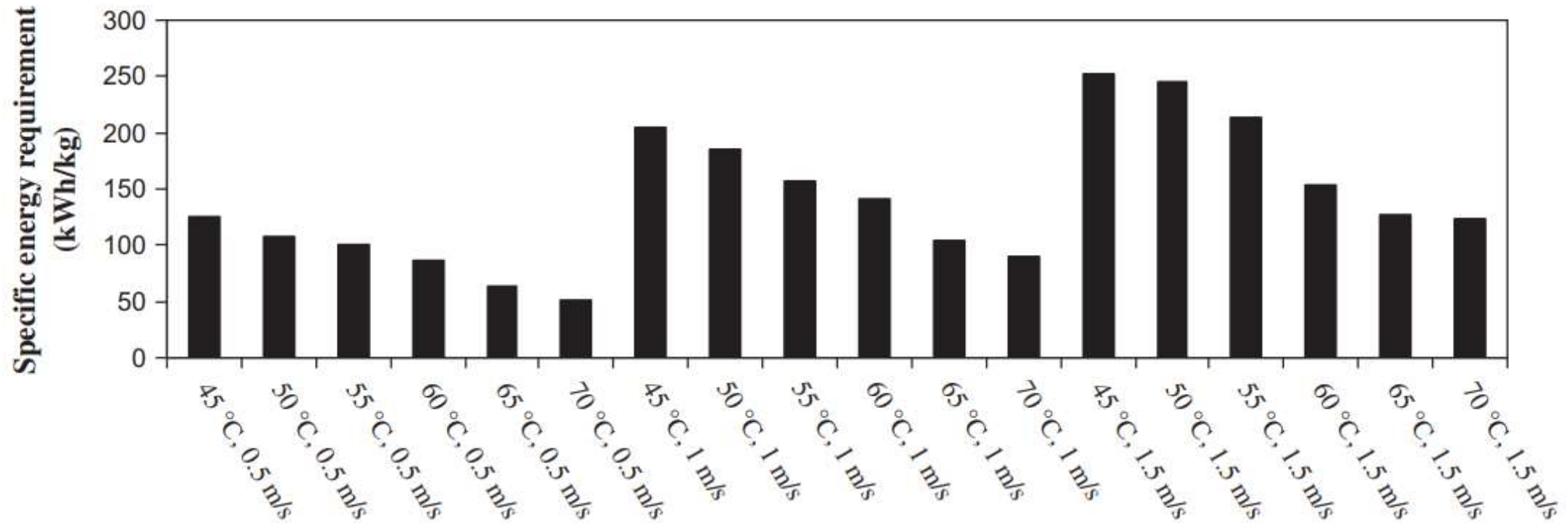


Fig. 4. Specific energy requirement for convection drying of arils (control treatment).

Key factors
influencing
drying
kinetics and
energy
consumption

Drying method and technology

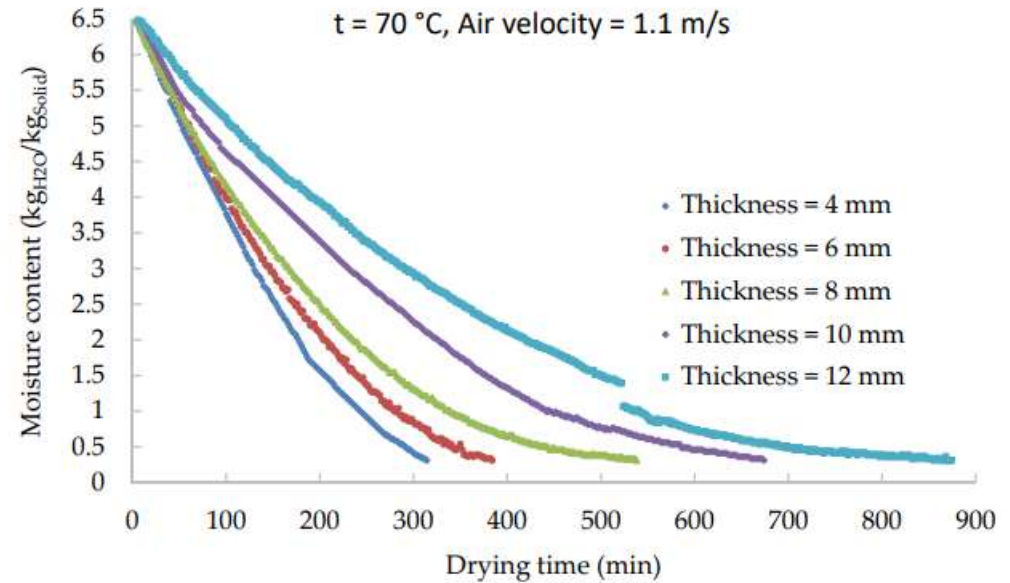
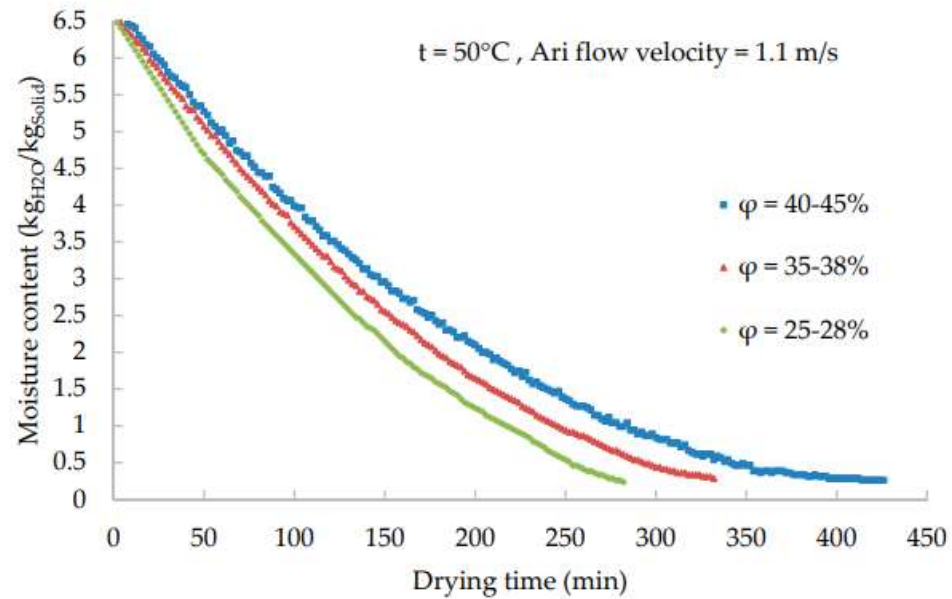
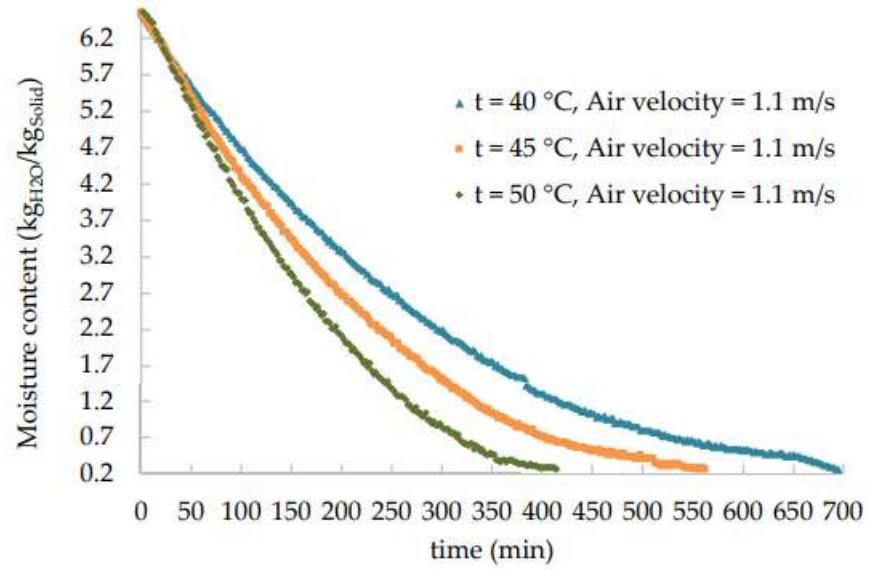
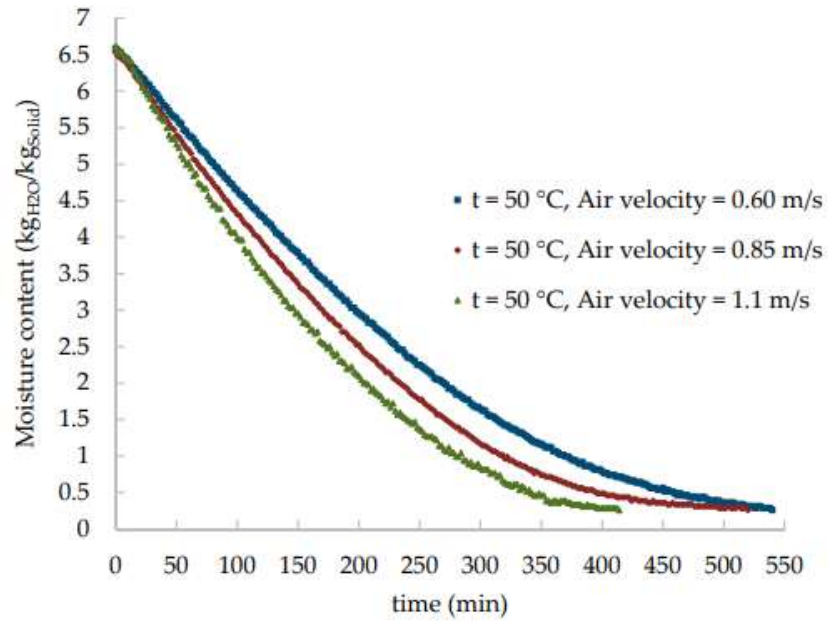
Air relative humidity

Air temperature

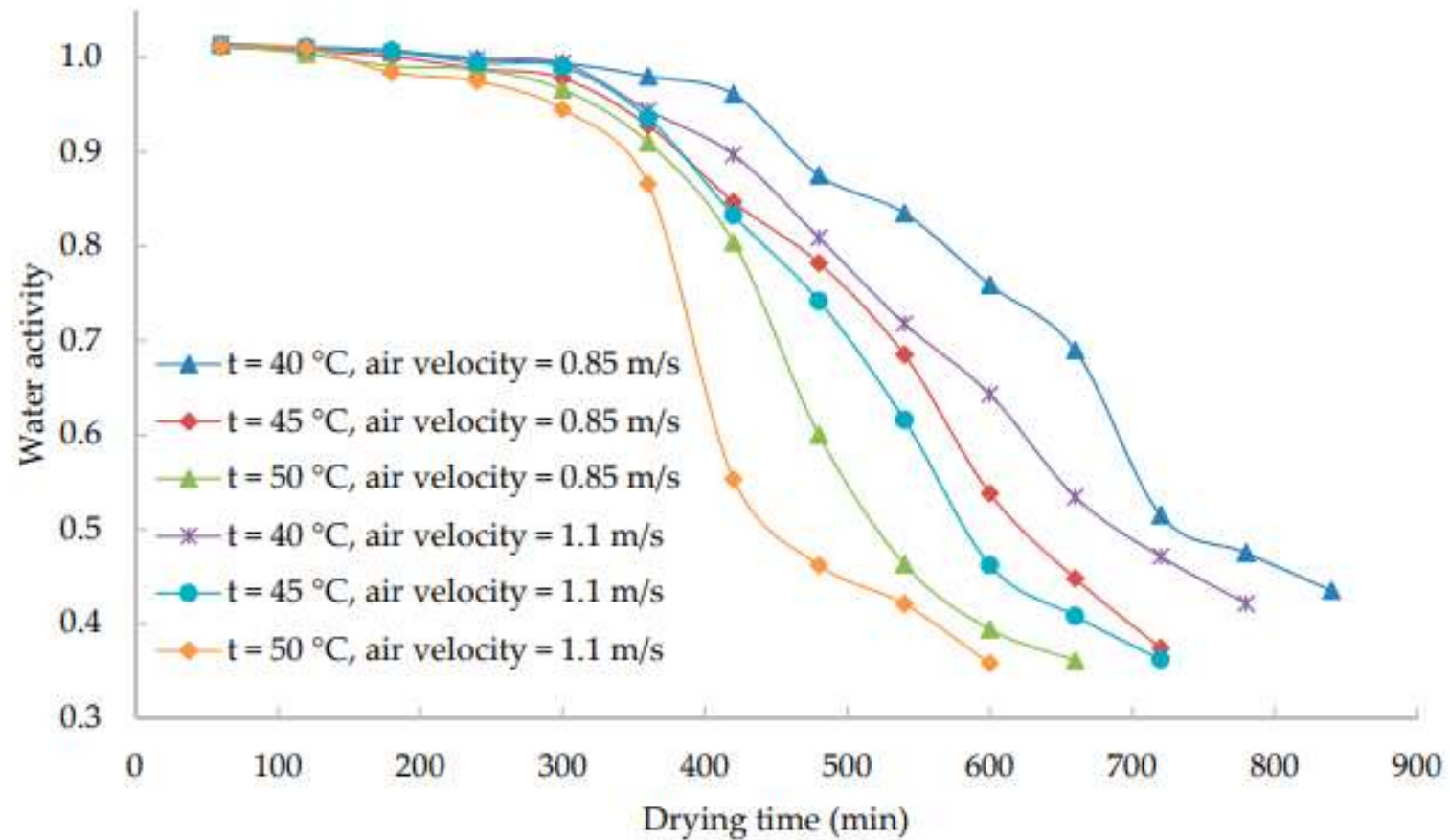
Air velocity

Sample characteristics

Pressure



Effect of process conditions on water activity



Prediction of drying kinetics by mathematical modelling

Two approaches:

1. Drying models employing the analysis of physical phenomena, such as mass diffusion, heat transfer, and surface tension

2. Empirical models based on experimental measurements

Macroscale Models

Heat transport equations

$$1 \quad \frac{\partial T}{\partial t} = \nabla \cdot (\alpha \nabla T)$$

$$2 \quad \frac{\partial T}{\partial t} = \alpha \left(\frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} \right)$$

$$3 \quad \frac{\partial T}{\partial t} = \alpha \left(\frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} + \frac{\partial^2 T}{\partial z^2} \right)$$

$$4 \quad \frac{\partial T(\xi, \tau)}{\partial \tau} = Le \frac{\partial^2 T(\xi, \tau)}{\partial \xi^2}$$

Momentum equations

$$13 \quad \rho \frac{\partial u}{\partial t} - \nabla \cdot \left(\eta + \rho \frac{C_p k^2}{\sigma \epsilon} \right) \cdot (\nabla u + (\nabla u)^T) + \rho u \cdot \nabla u + \nabla P = 0 \lim_{x \rightarrow \infty}$$

$$14 \quad \rho_a C_{pa} \left(\frac{\partial T}{\partial t} \right) + \nabla \cdot (-\lambda_a \nabla T_{\infty}) + \rho_a C_{pa} u \nabla T_{\infty} = 0$$

Mass transport equations

$$5 \quad \frac{\partial X}{\partial t} = \nabla \cdot (D_{eff} \nabla X)$$

$$6 \quad \frac{\partial X}{\partial t} = D_{eff} \left(\frac{\partial^2 X}{\partial x^2} + \frac{\partial^2 X}{\partial y^2} \right)$$

$$7 \quad \frac{\partial X}{\partial t} = D_{eff} \left(\frac{\partial^2 X}{\partial x^2} + \frac{\partial^2 X}{\partial y^2} + \frac{\partial^2 X}{\partial z^2} \right)$$

$$8 \quad \frac{\partial}{\partial t} \left(\frac{X}{T} \right) = \frac{\partial}{\partial \xi} \left(a_{11} J D \frac{\partial X}{\partial \xi} + a_{12} J D \frac{\partial X}{\partial \eta} \right) + \frac{\partial}{\partial \eta} \left(a_{21} J D \frac{\partial X}{\partial \xi} + a_{22} J D \frac{\partial X}{\partial \eta} \right)$$

$$9 \quad \frac{\partial X}{\partial t} = \frac{1}{T} \frac{\partial}{\partial r} \left(r \text{Def} \frac{\partial X}{\partial r} \right) + \frac{\partial}{\partial y} \left(\text{Def} \frac{\partial X}{\partial y} \right)$$

$$10 \quad C_m \frac{\partial \psi}{\partial t} + \nabla \cdot (-K_m \nabla \psi) = 0$$

$$11 \quad \frac{\partial X}{\partial t} + u \frac{\partial X}{\partial x} = D_{eff} \frac{\partial^2 X}{\partial x^2}$$

$$12 \quad (1 - \varphi) \rho_{sol} \frac{\partial X_{wet}}{\partial t} = \dot{m}_{pol}$$

Table 1. Selected thin-layer mathematical models.

Model name	Model
Page	$MR = \exp(-kt^n)$
Modified Page	$MR = \exp[-(kt)^n]$
Henderson and Pabis	$MR = a \exp(-kt)$
Two-term	$MR = a \exp(-k_0 t) + b \exp(-k_1 t)$
Two-term exponential	$MR = a \exp(-kt) + (1 - a) \exp(-kat)$
Midilli	$MR = a \exp(-kt)^n + bt$
Approximation of diffusion	$MR = a \exp(-kt) + (1 - a) \exp(-kbt)$
Verma	$MR = a \exp(-kt) + (1 - a) \exp(-gt)$

Development of a new Process Conditions Sensitive (PCS) thin-layer mathematical model of hot air convective drying



Chemical Engineering Communications



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Process conditions sensitive (PCS) thin-layer mathematical model of hot air convective drying

Juma Haydary, Mohammad Jafar Royen & Abdul Wasim Noori

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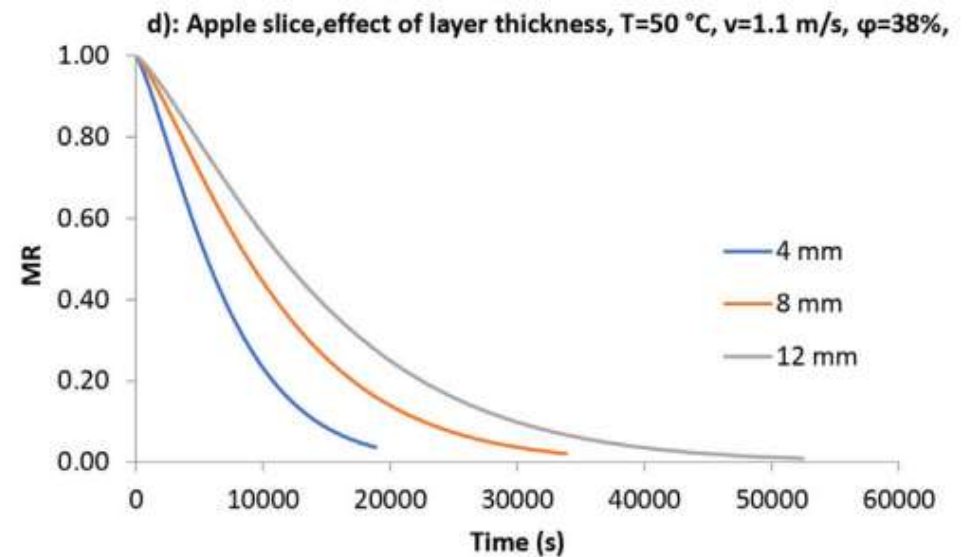
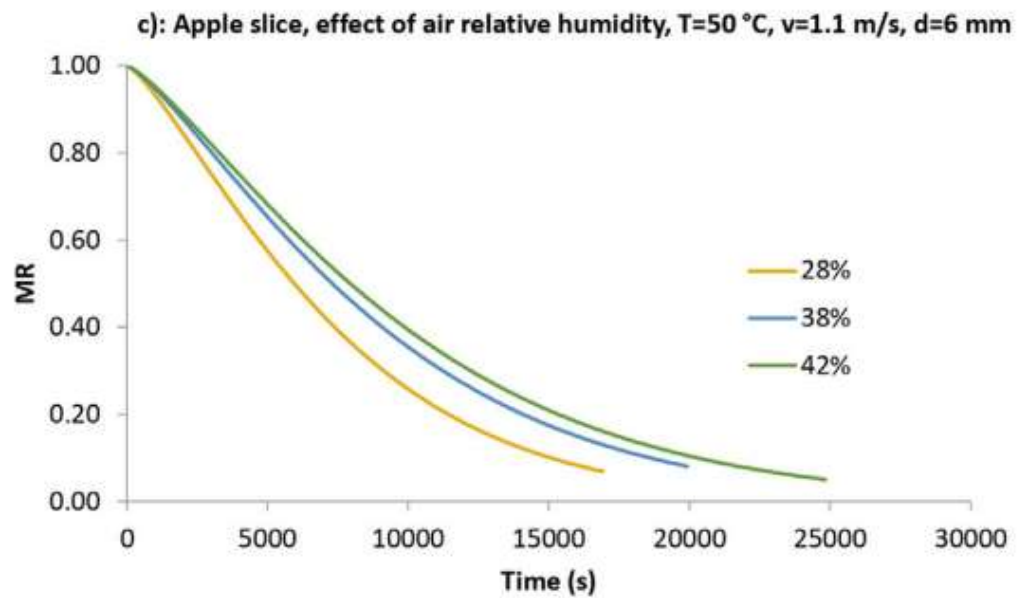
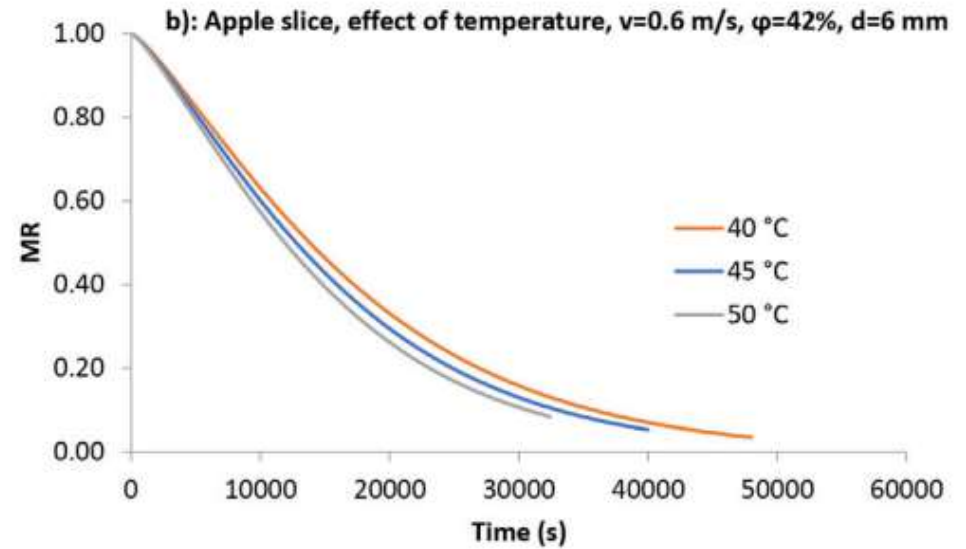
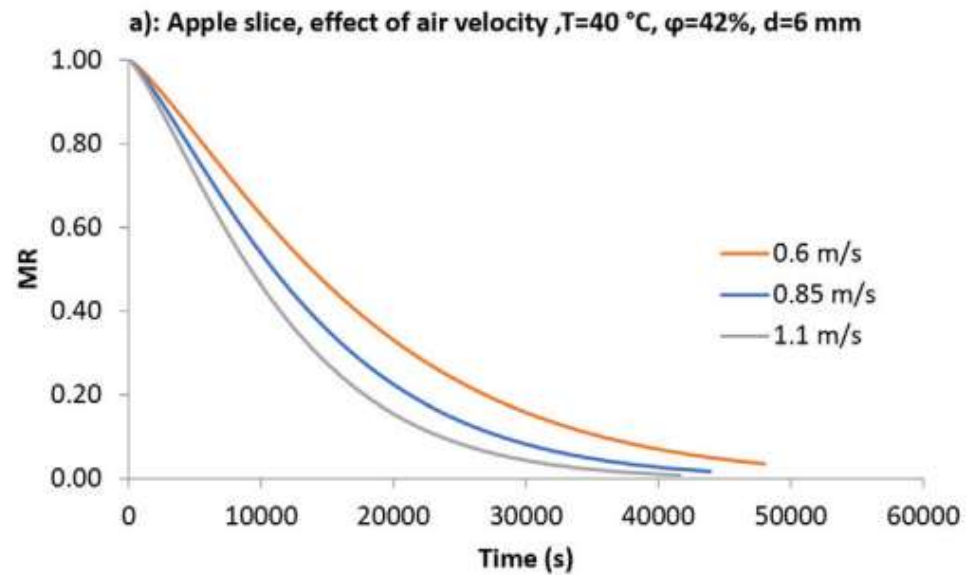
$$MR = \text{EXP}[-kF_k t^{nF_t}]$$

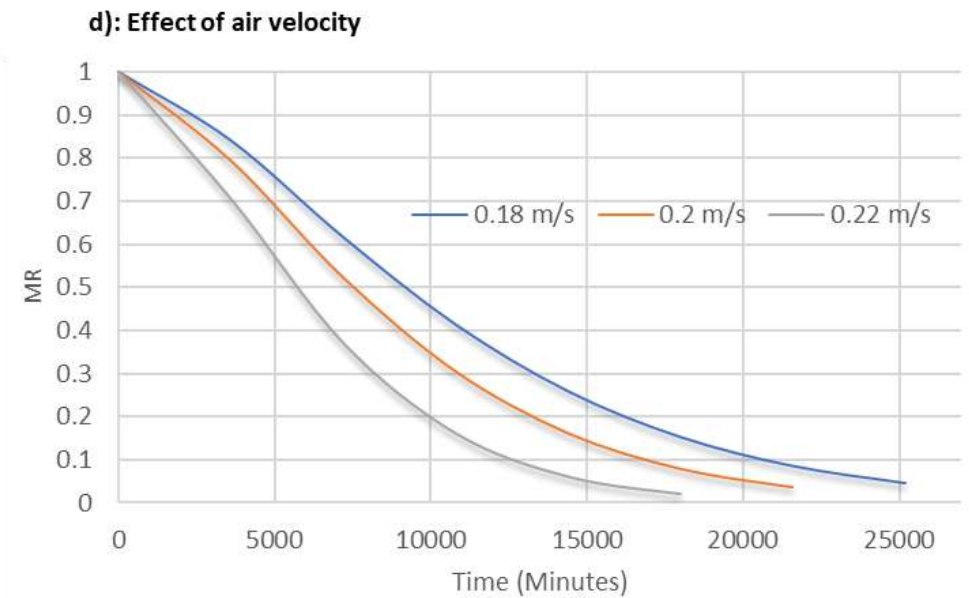
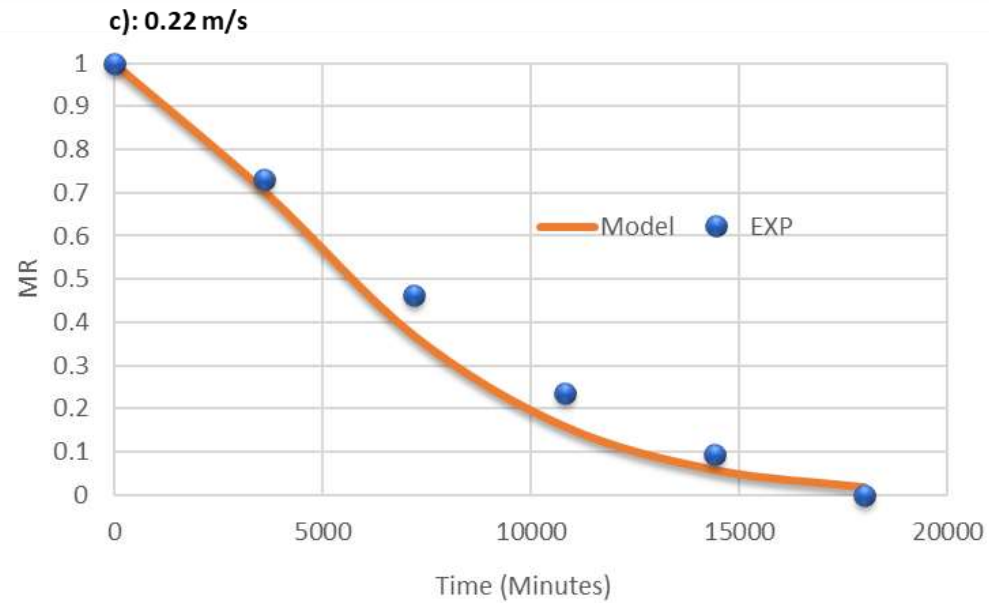
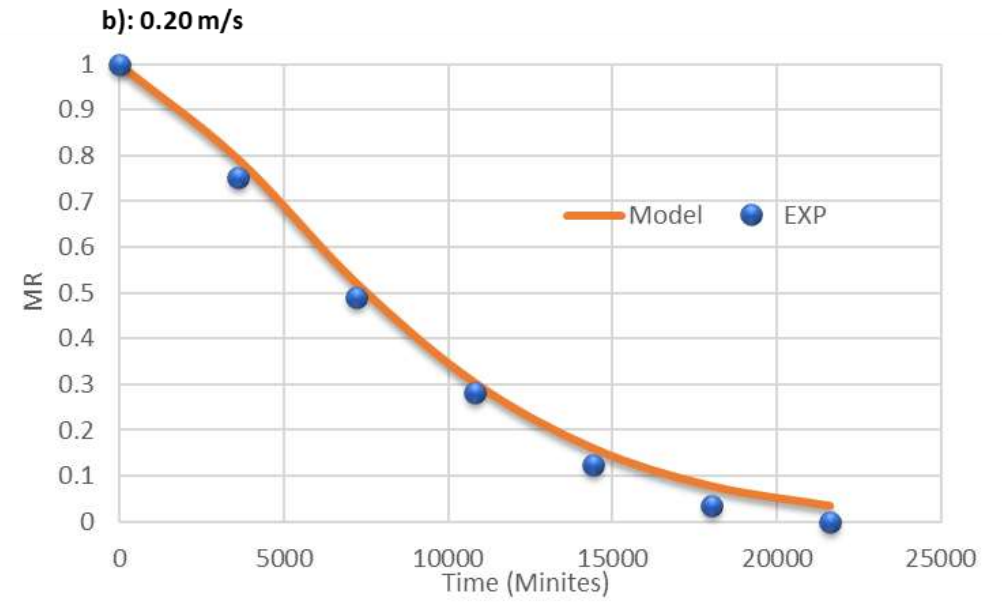
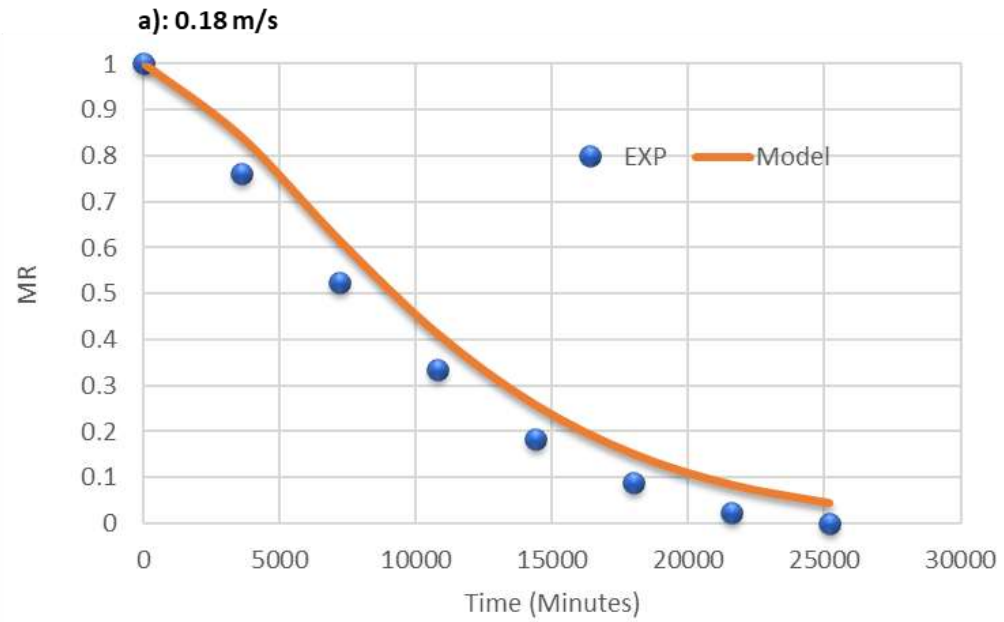
$$F_k = \left(\frac{T/T_{\min}}{d/d_{\min}} \frac{v/v_{\min}}{\varphi/\varphi_{\min}} \right)^p$$

$$F_t = \left(\frac{T/T_{\min}}{d/d_{\min}} \frac{v/v_{\min}}{\varphi/\varphi_{\min}} \right)^r$$

$$MR = \frac{M - M_e}{M_0 - M_e}$$

$$OF = \sum_T \left(\sum_i (MR_{Exp,i} - MR_{Pred,i})^2 \right)_{min} + \sum_v \left(\sum_i (MR_{Exp,i} - MR_{Pred,i})^2 \right)_{min} + \sum_\varphi \left(\sum_i (MR_{Exp,i} - MR_{Pred,i})^2 \right)_{min} + \sum_d \left(\sum_i (MR_{Exp,i} - MR_{Pred,i})^2 \right)_{min} = \min$$



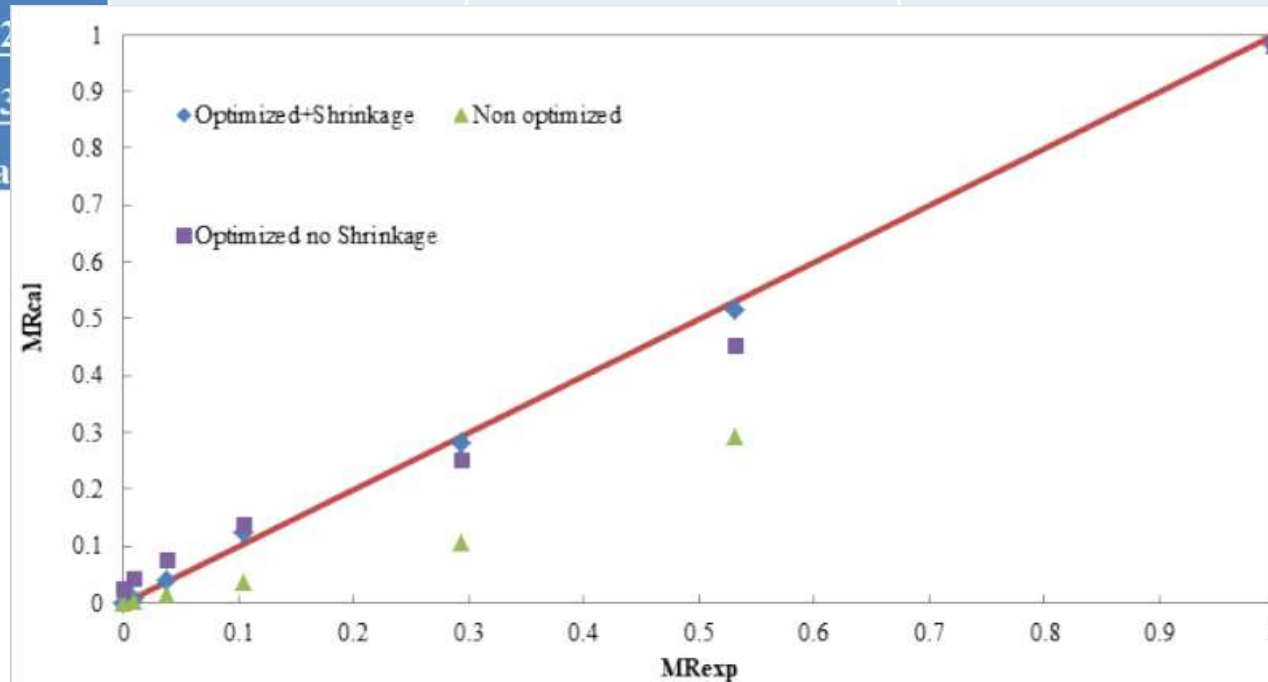


Effect of shrinkage

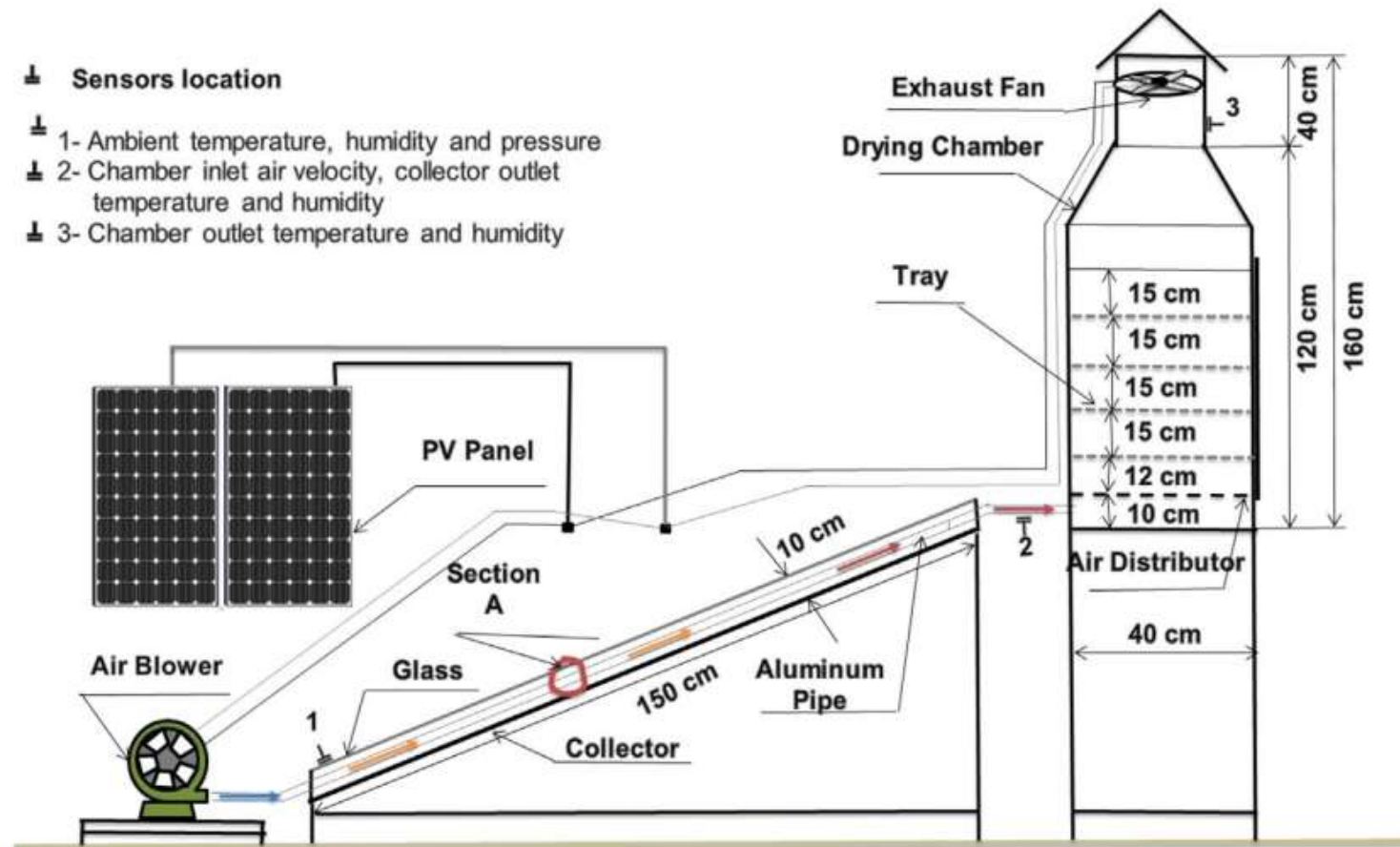
$$MR = \sum_{n=0}^{\infty} \frac{8}{(2n+1)^2 \pi^2} \text{Exp} \left(-\frac{(2n+1)^2 \pi^2 D_{eff} t}{4 l^2} \right)$$

Effective diffusion coefficient

D_{eff} (m ² s ⁻¹)	Non-optimized	Optimized shrinkage not considered	Optimized shrinkage considered
Day 1	6.10 10 ⁻¹⁰	3.30 10 ⁻¹⁰	2.33 10 ⁻¹⁰
Day 2			
Day 3			
Lab. Ba			

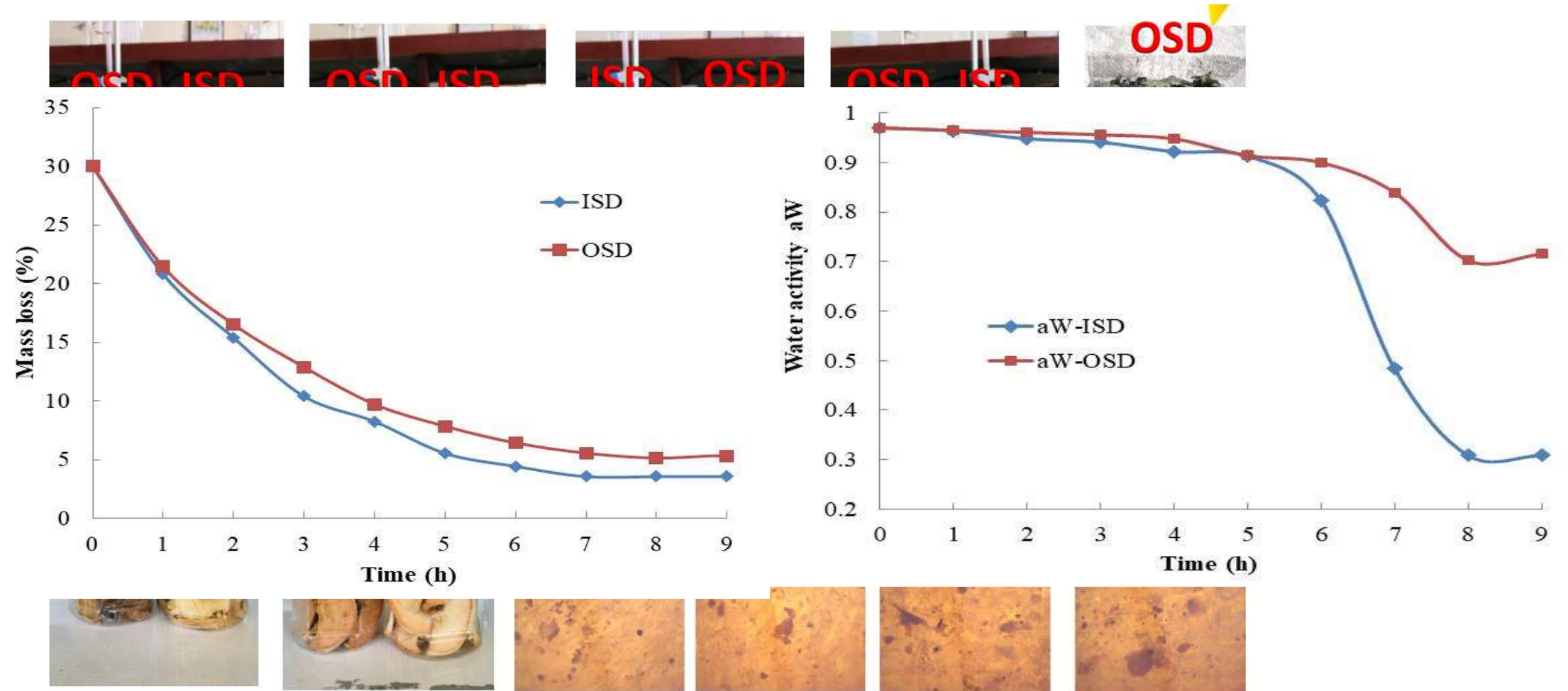


Use of renewable energy in food drying, solar drying

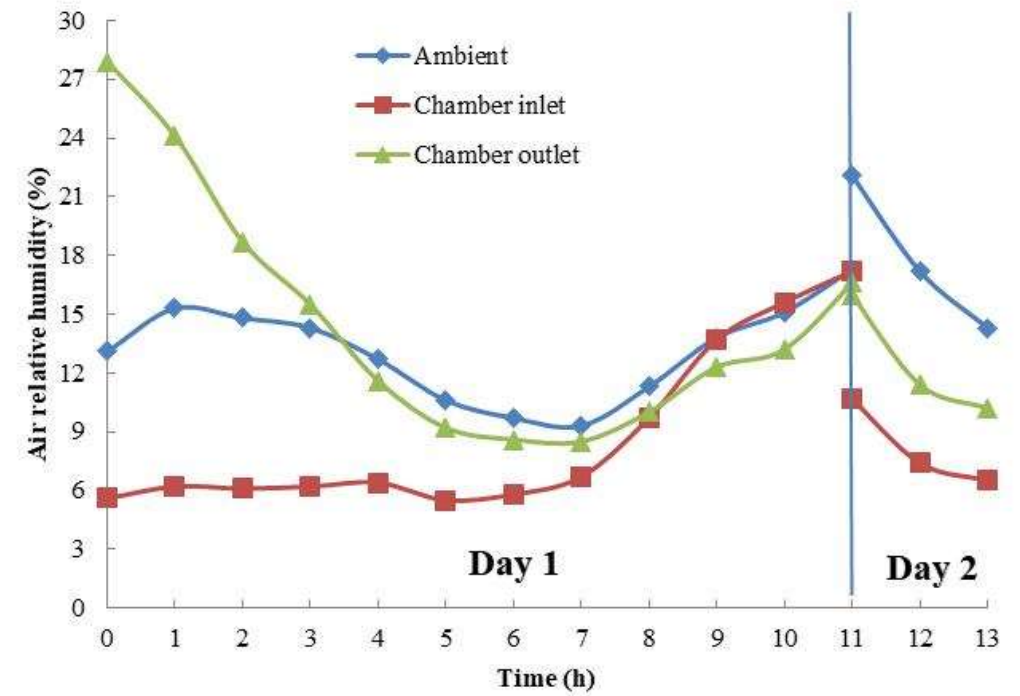
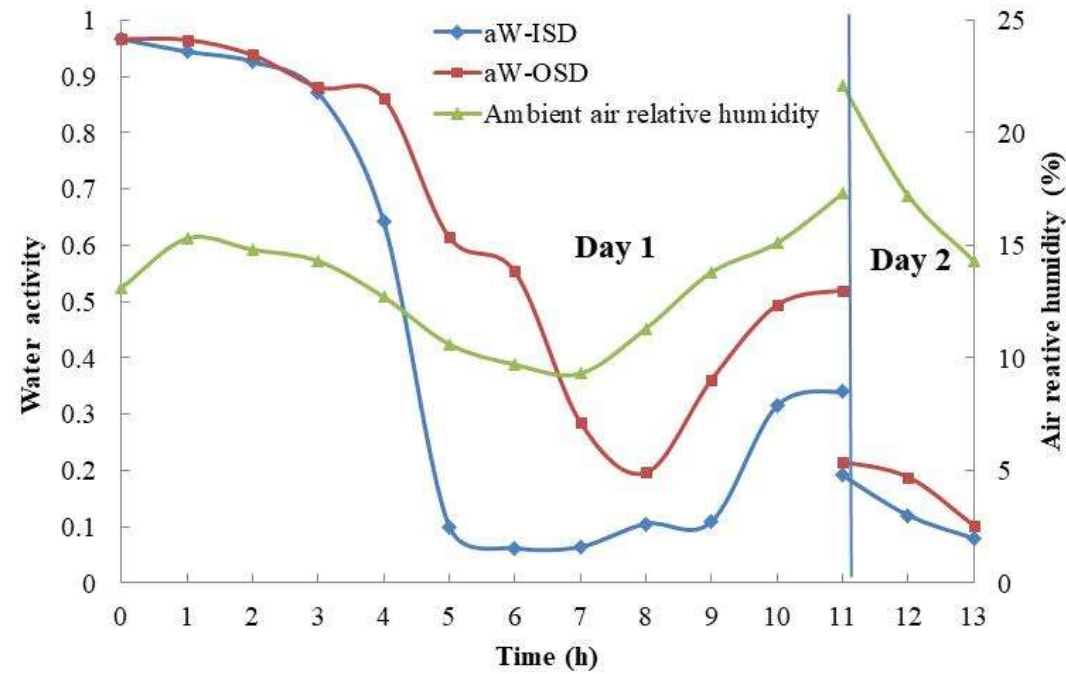


Indirect forced solar drying system

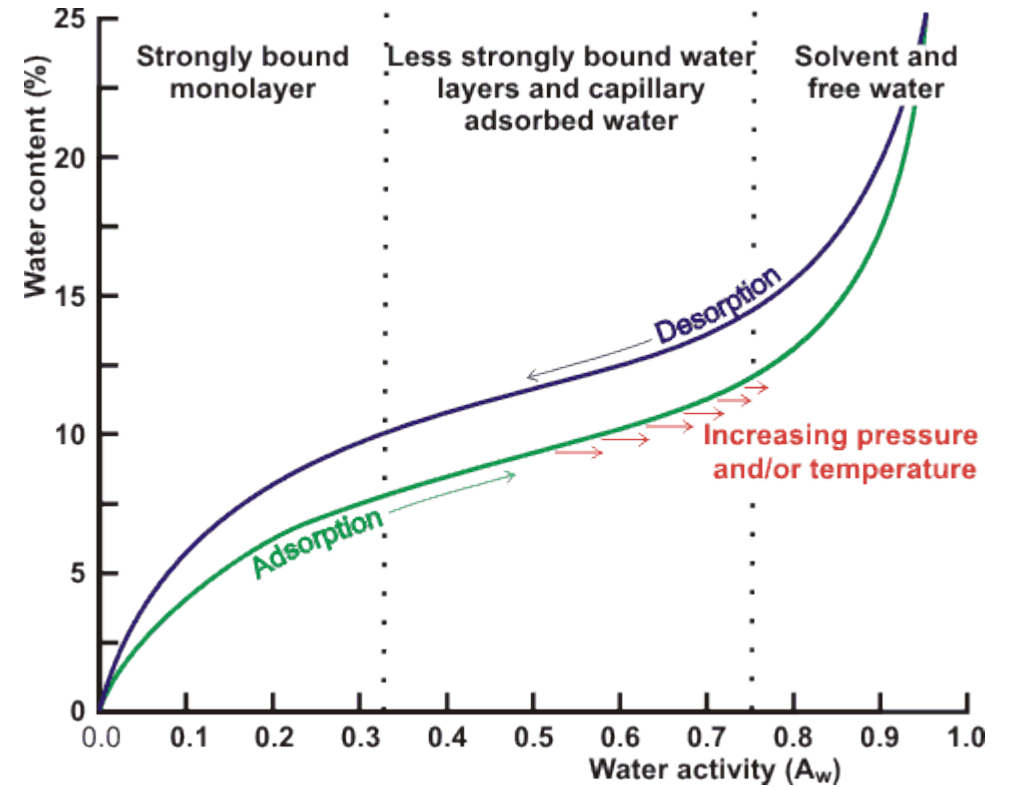
Why indirect solar drying?



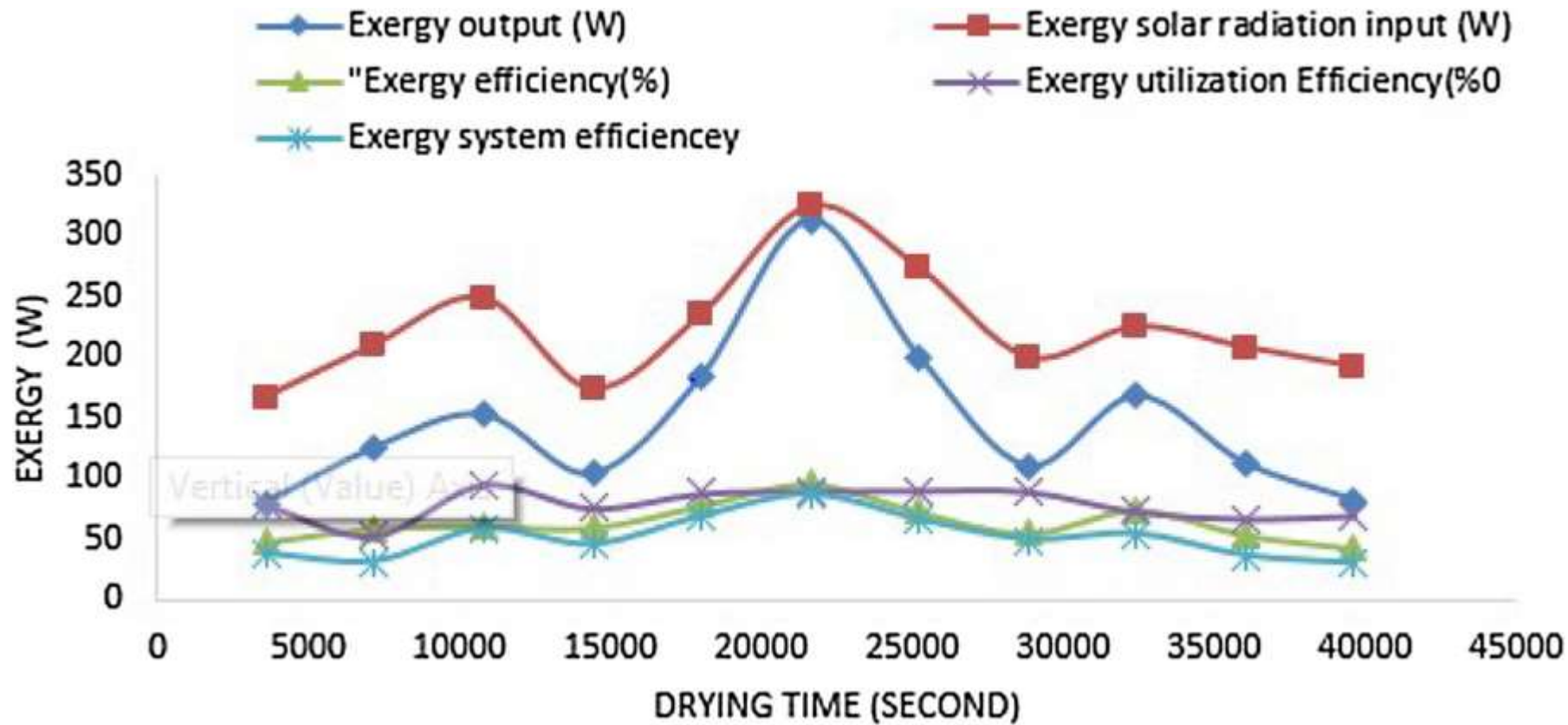
Effect of ambient air relative humidity



Rehydration of dried products



Energy efficiency of solar drying



Sintie, Y. T., & Aduye, G. T. (2020). Potential assessment and experimental analysis of solar vegetable dryer: in case of northern Ethiopia. *Renewables: Wind, Water, and Solar*, 7(1), 1-28.

Thank you for
your attention

